Optimization of PI Controller Gains in Nonlinear Controller of STATCOM Using PSO and GA

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Abstract— According to nonlinear operation of STATCOM, nonlinear controller has a better performance in comparison with linear controller. Regulating the DC capacitor voltage in STATCOM is a common task and can improve the system dynamic. The nonlinear control is based on exact linearization via feedback. A PI controller exists in this control system to regulate the capacitor voltage. In conventional scheme, the trial and error method has been used to determine PI controller coefficients. In this paper, the effect of PI gains on responses of $V_{dc}$, $I_d$ and Modulation Index (M) is presented. The exact calculation of optimized PI coefficients can be carried out to reduce disturbances and steady state error in DC link voltage. Therefore, in this paper, Particle Swarm Optimization (PSO) approach is used. It is shown that capacitor voltage tracks the reference value and vibrations are less than conventional status. Also, Genetic Algorithm (GA) has been used and compared with the results.

Index Terms— STATCOM, Nonlinear Controller, Optimized PI Coefficients, Particle Swarm Optimization and Genetic Algorithm

I. INTRODUCTION

STATic COMpensator (STATCOM) is a shunt Flexible AC Transmission System (FACTS) devices that can regulate line voltage at the Point of Common Coupling (PCC), balance loads or compensate load reactive power by producing the desired amplitude and phase of inverter output voltage. AC system is connected to a DC capacitor (energy storage device) through the inverter [1]. There are many possible configurations of Voltage Source Inverters (VSI) and consequently many different configurations of STATCOMs [2-3]. Many different control strategies such as Proportional-Integral (PI) controller, sliding mode controller [4] and nonlinear controller have been suggested to control STATCOM. Because of nonlinear operation of STATCOM, nonlinear controller is preferred over linear controller [5]. Moreover, in linear controller, four chosen sets of PI parameters may not be suitable for all ranges of operating points and finding these values are very time consuming and complex [6-7]. In nonlinear controller, the Generalized Averaged Method [8] has been used to determine the nonlinear time invariant continuous model of the system [9-11]. This model has been used to present a nonlinear control law based on exact linearization via feedback for STATCOM [12]. This method is particularly interesting because it transforms a nonlinear system into a linear one in terms of its input-output relationship. In [9-10], only $q$ axis current has been regulated, but it should be noted that unlike other shunt compensators, large energy storage device that have almost constant DC voltage, makes STATCOM more robust and it also enhances the response speed. Therefore, there are two control objectives implemented in STATCOM. First one is $q$-axes current and the second objective is capacitor voltage in DC link [13]. The $q$-axes current tracks its corresponding reference value perfectly, but the capacitor voltage ($V_{dc}$) is not fixed on reference ideally because of presence of a PI controller between the reference of the d-axes current ($I_d$) and $V_{dc}$ error ($V_{dc} - V_{dc}$). In other words, the performance indices (settling time, rise time and over shoot) have notable values. Thus, the optimized and exact determination of PI controller gains can lead to the reduction in system disturbances.

In this Paper, two well-known optimization methods (e.g., GA [14-15] and PSO [19-20]) are applied to find optimized values of PI gains and compare with each other. Two objective functions are defined. The determined PI coefficients are implemented in the controller to demonstrate the improvement of the convergence speed, reduction of error, the overshoot in the capacitor voltage and other circuit parameters. The results are compared with trial and error method, too.
II. CONFIGURATION OF STATCOM

In this paper, a simplified STATCOM configuration, shown in Fig. (1), is considered. It consists of a voltage source inverter, a capacitor, C, an inductance, L (representing the leakage inductance of the transformer and line) and a resistor, R_s (representing the inverter and transformer conduction losses) on the AC side.

\[ V_a, V_b, V_c \] are called line voltages. \( E_a, E_b, E_c \) are the inverter output voltage and \( V_{dc} \) is the DC voltage.

![Figure 1. Representation of STATCOM](https://doi.org/10.24084/repqj08.276)

The angular velocity of the AC voltage and current vectors is \( \omega \). Let us consider a system of reference \( (d, q) \) rotating at the same speed, and let us note \( \alpha \) to be the angle between \( d \) axis and line voltage vector \( (E) \). The system equations are as follows [9]:

\[
\begin{bmatrix}
\frac{dI_d}{dt} \\
\frac{dI_q}{dt}
\end{bmatrix} = \begin{bmatrix}
\frac{-R_s}{L_s} & -\omega \\
\omega & -\frac{R_s}{L_s}
\end{bmatrix} \begin{bmatrix}
I_d \\
I_q
\end{bmatrix} + \frac{1}{L_s} (V_{dq} - E_{dq})
\] (1)

The powers are expressed by equation (2):

\[
P = \frac{3}{2} (E_d I_d + E_q I_q), \quad Q = \frac{3}{2} (E_d I_q - E_q I_d)
\] (2)

If \( \alpha \) is chosen by zero, the \( E_q \) voltage will be equal to zero and the reactive power becomes proportional to \( E_d I_q \). To control the reactive power (Q), it is sufficient to control \( I_q \).

\[
E_q = 0, \quad Q = \frac{3}{2} E_d I_q
\] (3)

\[
P = V_{dc} C \frac{dV_{dc}}{dt}
\] (4)

Rewriting the Eq. (2) for capacitor voltage and substituting Eq. (4) in it, results in the third equation will be added to other two equations of Eq. (1).

By applying the Averaged Model used for control, only fundamental component of inverter output voltage is considered. The influence of all other harmonics is ignored.

The control variable is the firings angle (\( \delta \)) with reference to the network voltage zero crossing(\( E_j \)). This model is used to simulate the system, but not to choose and tune the controller. A Generalized Averaging method [8] is used to get a continuous time invariant model of the converter. So, the averaged equations are as follows:

\[
\frac{d}{dt} \begin{bmatrix}
I_d \\
I_q \\
V_{dc}
\end{bmatrix} = \begin{bmatrix}
-\frac{R_s}{L_s} & \omega & -M \cos \delta \\
-\omega & -\frac{R_s}{L_s} & -M \sin \delta \\
M \cos \delta & M \sin \delta & 0
\end{bmatrix} \begin{bmatrix}
I_d \\
I_q \\
V_{dc}
\end{bmatrix}
\] (5)

III. NONLINEAR CONTROL SCHEME FOR STATCOM

The nonlinear control law is based on the theory of exact linearization via feedback [12]. In this law, the system has to be described by Eqs. (6-7). It is relative degree \( r \) if Eqs. (9-10) are verified for all \( x \) and all \( k < r - 1 \). \( L_f h(x) \) is called \( h(x) \) derivative along \( f \); it is defined by equation (8).

\[
x = f(x) + \sum_{i=1}^{m} g_i(x) u_i
\] (6)

\[
y_1 = h_1(x)
\] (7)

\[
L_f h(x) = \frac{\partial h(x)}{\partial x} f(x)
\] (8)

\[
\begin{bmatrix}
l_{g_1} L_f h_1(x) \\
l_{g_2} L_f h_2(x) \\
\vdots \\
l_{g_m} L_f h_m(x)
\end{bmatrix} = 0
\] (9)

\[
l_{g_i} L_f h_i(x) \neq 0 \text{ for at least one } 1 \leq j \leq m
\] (10)

For STATCOM system, because of compensating the reactive power and eliminating the undesired internal dynamic, \( Q \) and \( V_{dc} \) are chosen as output control variables. Consequently, the \( M \) and \( \delta \) are chosen as two control inputs variables. So, a MIMO system is obtained as follows:

\[
\dot{X} = f(x) + g_1(x) u_1 + g_2(x) u_2 =
\] (11)

\[
Y = \begin{bmatrix}
h_1(x) \\
h_2(x)
\end{bmatrix} = \begin{bmatrix}
x_1 \\
x_2
\end{bmatrix}
\] (12)

Where \( X \) and \( U \) are state and input control vectors, respectively.

\[
X = \begin{bmatrix}
x_1 \\
x_2 \\
x_3
\end{bmatrix} = \begin{bmatrix}
I_d \\
I_q \\
V_{dc}
\end{bmatrix} \text{ is state vector}
\]

\[
U = \begin{bmatrix}
u_1 \\
u_2
\end{bmatrix} = \begin{bmatrix}
M \cos \delta \\
M \sin \delta
\end{bmatrix} \text{ is input control vector}
\]

The system described by equations (11-12) has a relative degree of \( r = [1,1] \), and a fairly standard form. Solving the problem of reproducing a reference output, results in the following control law:
The control law and three controllers is modeled. Thus, the system with nonlinear inputs.

The general principles for the PSO algorithm are shown in Fig. 2. Thus, the system with nonlinear inputs.

For the STATCOM system, the adopted objective function is presented by the following equation:

\[ J_{\text{ITAE}} = \int_0^T t |e(t)| \] (18)

Where the upper limit \( T \) is a finite time chosen so that the integral approaches a steady-state value and is usually chosen as the setting time \( T_s \).

For the STATCOM system, the adopted objective function is presented by the following equation:

\[ Q_f(Z) = \sum_i m_i f_i(Z) \] (19)

Where

\[ f_i(Z) = \sum_j \omega_j \int_0^T |e_j(t)| \] (20)
For the STATCOM, two objective functions are defined. The objective function deduced by Eq. (18) is expressed by the following equations:

\[ Q_f(Z) = 1000 \int_0^T |tV_{dc}(t) - V_{dc,REF}| + t|I_d(t)| \]  
\[ Q_f(Z) = f(Z) = 1000 \int_0^T |tV_{dc}(t) - V_{dc,REF}| \]  

Where,  
\[ Z = [K_p \ K_I] \]

The Eq. (21) is used when the goal is controlling both the \( V_{dc} \) and \( I_d \) which is named double objective function. Eq. (20) should be used when \( V_{dc} \) is individually regulated which is named single objective function.

V. SIMULATION RESULTS

The case study parameters of the system, shown in Fig. 1, are as follows:

\[ C=490 \, \mu \text{F}, F=50 \, \text{Hz}, R=28 \, (\Omega), L=0.0013 \, (\text{H}), V_d=110 \, \text{Vrms}(L-L) \, (\text{V}), V_{dc}=200 \, (\text{V}), \text{Initial voltage}=200 \, \text{V} \]

The reference \( I_r \) has a step change from zero to 15A at \( t=0.02 \, \text{s} \). \( \lambda_1 \) and \( \lambda_2 \) are selected equal to 1000.

In this section, the effect of PI gains on voltage regulation is shown by using unsuitable PI gains. Then PI gains, computed through trial and error method, are compared with ones computed by PSO with two objective functions and finally the results of PSO are compared with the results GA.

Randomly, 0 and 10 are selected for \( K_p \) and \( K_I \), respectively. Fig. 3 shows the \( V_{dc} \) response.

![Capacitor voltage response to random PI gains](image1)

Figure 3. Capacitor voltage response to random PI gains

It is obvious that these values result in divergence and are improper for controlling the STATCOM. Consequently, PI coefficients cannot be determined randomly. The ordinary solution method for determination of PI gains is trial and error method. Many pairs should be tested. Then the best of them are selected. Some benchmarks such as steady state error and fluctuations are effective in choosing PI gains. Every one may select a unit pair and there is no good performance guaranty for them. Here, a set of forty pairs are studied and finally PI gains are selected to be \( K_p=1 \) and \( K_I=70 \). In PSO method, the number of population and iteration are 20 and 200, respectively. The objective functions are given by Eqs. 21 and 22. The calculations are offline; therefore the running time (about 20 minutes) is not important. The three PI pairs from trial and error, single-objective (Eq. 22) PSO and double objective (Eq. 21) PSO methods have been applied to STATCOM. The corresponding time domain simulation plots for \( V_{dc}, I_d, M, \delta \) and \( I_r \) have been compared in figures (4)-(7). As shown in Fig. 4, the best regulation of \( V_{dc} \) is obtained by PSO with single and double objective functions. The overshoot is very small and voltage is approximately fixed on 200V. But as it was predicted, the performance of single-objective function is better and double objective function response has a teeny steady state error. The presence of high frequency fluctuations in single-objective function response causes \( I_d \) and \( M \) to reach to their corresponding nominal values with high frequency fluctuations (see Figs. 5 and 6). Thus if the objective is to reduce oscillations in addition to voltage regulation, the double-objective function has a relative superiority over single-objective function and has to be chosen. The results of implementing double-objective function are shown with black color in Figs. (4-7). Double-objective function completely removes high frequency oscillations from \( I_d \) and \( M \) responses and converges with higher speed. All methods have a nearly same \( \delta \) and \( I_r \) responses (Fig. 7).
VI. COMPARISON BETWEEN PSO AND GA

In this section, GA [18] is employed and compared with PSO. The results of running GA and PSO are used in Table 1.

Comparison between two methods with a same function shows that PSO results in fitness function with lower value. Figures 8-10 compare PSO and GA for $V_{dc}$, $I_d$ and $M$ responses with two types of objective functions.

<table>
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<th>Table 1. Results of PSO and GA</th>
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<td><strong>Method</strong></td>
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In Fig. 9, PSO response has more disturbances but faster convergence speed in the case of optimization of Vdc & Id. Generally, PSO responses have less fluctuation in comparison with GA responses in the case of optimization of Vdc. In the case of optimization of double-objective function for PSO, Vdc response reaches to steady state with higher speed and less fluctuation, Id response reaches to steady state with higher speed and more fluctuations and M response has not a good performance in comparison with GA responses.

VII. CONCLUSION

The nonlinear control method of the STATCOM which is based on the exact linearization via feedback has a proportional–integral controller with unknown PI parameters which they have a remarkable influence on responses of system variables such as line current, M and DC link voltage. Traditional solution is the calculation of these coefficients by using trial and error method. In this paper, PSO with two types of objective function has been used in determination of PI parameters and compared with GA. It is shown that the PSO method leads to a better regulation of DC link voltage, d and q axis currents and other circuit parameters. Also, the time of reaching to steady state value, settling time the fluctuations and overshoot have been decreased, too.

VIII. REFERENCES