

Geothermal Hot Water and Space Heating System in Egypt

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Abstract Direct utilization of geothermal energy refers to the immediate use of the heat energy rather than to its conversion to electrical energy. The primary forms of direct use include heating and cooling. Geothermal energy could be used to supply hot water or could be used with a special equipment (radiators) to make buildings warmer during winter seasons. In general, the geothermal fluid temperatures required for direct heat use are lower than those for economic electric power generation. Most direct use applications use geothermal fluids in the low-to-moderate temperature range between 50o and 150oC. Although Egypt is not characterized by abundant igneous activity, its location in the northeastern corner of the African plate suggests that it possess geothermal resources, especially along its eastern margin. The data indicate that the temperature of 150 oC may be found in the reservoir in the gulf of Suez and red coastal zone. This work designs a geothermal hot water and space heating system to operate in three buildings in a remote area in the Eastern Desert (i.e. school, home & emergency hospital) and applies to the Umm Huweitat well(sample no. 69 on the Red Sea approximately 20 km north of the city of Safaga.) as a case study.

Keywords

Geothermal energy, production well, heat exchanger, radiator, water heater

1. Introduction

Geothermal energy is energy derived from the heat of the earth's core. It is clean, abundant, and reliable. If properly developed, it can offer renewable and sustainable energy source. After the Second World War many countries were attracted by geothermal energy, considering it to be economically competitive with other forms of energy. It did not have to be imported, and, in some cases, it was the only energy source available locally. Geothermal energy utilization is divided into electric energy production and direct uses. Direct utilization of geothermal energy consists of various forms for heating and cooling instead of converting the energy for electric power generation [1]. The major areas of direct utilization are: heating of swimming pools and for space heating and cooling including district heating; agriculture

applications (greenhouse heating and crop drying); aquaculture applications; industrial processing; and geothermal heat pumps.

In general, the geothermal fluid temperatures required for direct heat use are lower than those for economic electric power generation. The geothermal resources in Egypt are in the lower temperature ranges that are more widespread than the higher temperature resources that may be found in the reservoir in the gulf of Suez and red coastal zone [2]. In this context, the proposed work presents and design a geothermal hot water and space-heating system designed to operate in three different buildings (i.e. school, home & emergency hospital) in a remote area in the Eastern Desert of Egypt.

2. The Proposed Geothermal Hot Water and Space Heating System Components

The block diagram of the geothermal hot water and space heating system is shown in Fig. 1. The diagram consists of a production facility (Umm Huweitat well (sample no. 69) throughout the Eastern Desert) to convey the heated water to the surface, a mechanical system (piping, pump, controls) to convey the heat energy to where it is required, a disposal system to receive the output fluid, a heat exchanger to minimize possible corrosion, scaling, or fouling of pipes, valves and other fittings in the system, radiators to make buildings warmer during winter seasons and simple geothermal water heaters for supplying hot water.

3. System Design

The design and the selection of each component of the geothermal hot water and space heating system plays an important role in the system reliability, safety, cost and maintenance. Size, type and material of each component are the most important parameters, which should be considered.

A. Design of the space heating system

a. Space heating load calculation

Before designing a heating system, one must estimate the amount of heat which is lost from the building. There are two sources of heat loss from a building fabric heat losses and ventilation heat losses. Fabric heat losses are losses directly through the walls, windows, doors, floors and ceiling of the room. For ease of calculation, it is assumed that these losses are at a uniform rate through each surface. The heat loss (Qf) rates are obtained by multiplying the area of each individual surface (As) by the design temperature difference (ti-to) and the heat transfer co-efficient called the 'U' Value. [3].

Thus;

$$Q_f \text{ (k.cal/hr)} = A_s \text{ (m}^2\text{)} * (t_i - t_o) \text{ (}^\circ\text{C)} * 'U' \text{ Value (k.cal/hrm}^2\text{. }^\circ\text{C)} \quad (1)$$

Ventilation heat losses are caused by the air flowing through a building. Ventilation rates are usually quoted in air changes per hour. Defined as the volume of the air flowing through the room in one hour divided by the actual volume of the room itself. This air clearly needs to be heated by the space heating system and the heat required (Qv) is calculated by multiplying the volume of the room(C) by the air change rate(ACH), the temperature difference between outside and inside(ti-to) and by the heat capacity of air (HCA) [3].

Thus;

$$Q_v \text{ (kcal/hr)} = C \text{ (m}^3\text{)} * \text{ACH} * (t_i - t_o) \text{ (}^\circ\text{C)} * \text{HCA (kcal/ hr. m}^3\text{. }^\circ\text{C)} \quad (2)$$

b. Design of radiators

There are different types of radiators (i.e cast iron, steel and aluminum radiators).A summary of typical ratings for different types of radiators for a temperature difference, water to air, of 60

oC is included in Table 1. These ratings may be corrected using Table 2 for 30 oC as in case of our application.

The most commonly used type is the steel radiators. The particular merits of steel radiators result from their small mass and their comparatively narrow waterways. They are light to handle on a building site and respond quickly to temperature control. Two types are selected to be used in our application, the radiant panel type for small rooms and a tubular type for medium and large rooms.

Fig.2 shows the two types. The heat load curves for the three buildings are put in the same diagram as shown in Fig.3.

B. Design of Water heaters

A small steel heat exchanger inside a stainless steel tank, as shown in Fig.4. transfers heat from the geothermal water to the domestic hot water. The tank consists of steel cylindrical vessel insulated by a layer of 7 cm of glass wool and the other casing cover is aluminum. The daily hot water consumption for the three buildings is shown in Table3.

Water heating load level shown in Fig.5 is influenced by

- The equipment: The dimension and the load level of the distribution tanks, and the insulation of tanks
- The user activities and the habits related to the different activities (for how long, how much water one use). Table shows the hot water consumption for the three buildings and the corresponding maximum heat load.

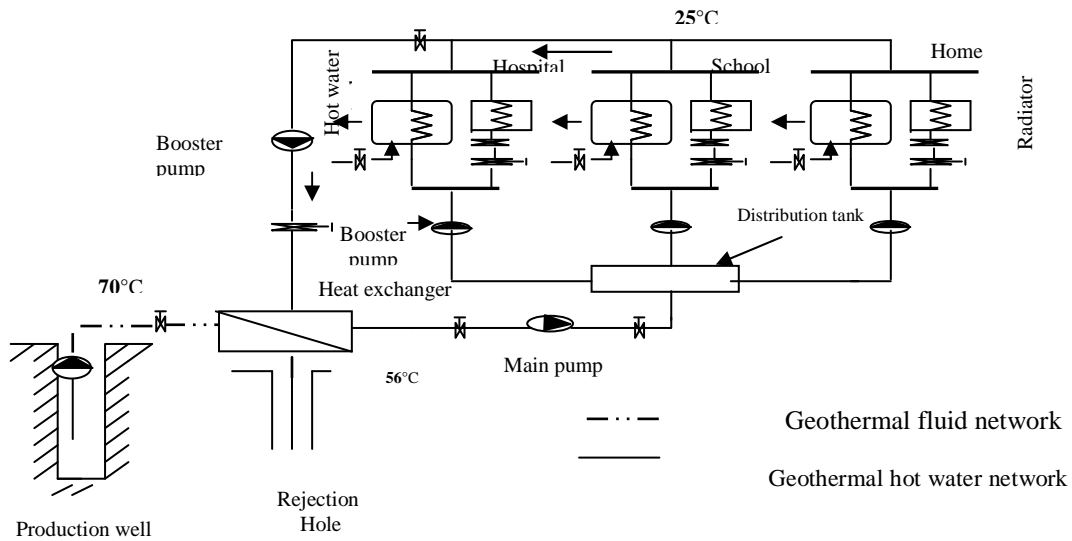


Fig.1 The geothermal hot water and space heating system

Table 1 Emissions from radiators for a temperature difference air to mean water of 60 °C[4].

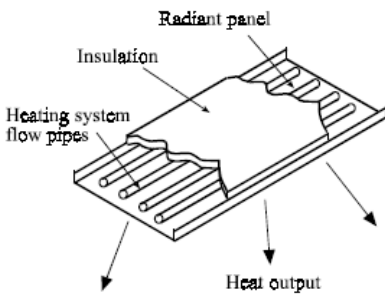
Radiator		Dimensions (mm)		Range of emissions of elevation (k.cal/hr .m ²)*10 ³
Type	pattern	Depth	Range of heights	
Cast iron sectional (open)	2- column	70	430-980	1.61-1.80
	4- column	160	430-980	2.93-3.08
	6- column	250	280	4.67
Cast iron sectional (flat front)	2- column	71	430-980	1.97-1.99
	4- column	161	430-980	3.45-3.5
	6- column	251	280	5.17
Radiant panel		35	500-900	0.99-1.04
Steel tubular with headers	40 mm crs for elements	98	400-1000	2.52-2.68
		166	400-1000	4.44-4.55
	60 mm crs for elements	98	400-1000	1.68-1.8
		166	400-1000	2.95-3.04
Aluminum sectional with flat panel front	Open top	95	430-690	3.89-4.0
	Closed top	160	285-435	5.74-5.79
Aluminum finned unit in casing	With damper at base	30	300-750	2.51-2.55

Table 2 Correction factors for power emitted from radiators [4].

$\Delta t(^{\circ}\text{C})^1$	0	1	2	3	4	5	6	7	8	9
30	0.41	0.43	0.44	0.46	0.48	0.49	0.51	0.53	0.55	0.57
40	0.59	0.61	0.63	0.65 ²	0.67	0.69	0.71	0.73	0.75	0.77
50	0.79	0.81	0.83	0.85	0.87	0.9	0.92	0.94	0.96	0.98
60	1.00	1.02	1.04	1.07	1.09	1.11	1.13	1.16	1.18	1.2
70	1.23	1.25	1.27	1.30	1.32	1.34	1.37	1.39	1.41	1.43
80	1.45	1.48	1.50	1.52	1.55	1.57	1.59	1.62	1.65	1.67

¹Temperature difference air to mean water

² Correction factor at temperature difference (Δt) =43^oC



(a) Radiant panel.

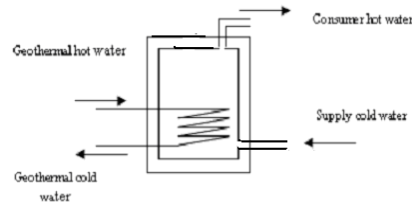


Fig. 4 Geothermal water heater.



(b) Steel tubular with headers

Table 3 Daily hot water consumption for the three buildings

Building	No of persons	Hot water consumption / person	Total consumption
Home	5 person *8 flat	30 liter/day	1200 liter/day
Hospital	30	30 liter/day	900 liter/day
School	100	5 liter/day	500 liter/day

Fig.2 Steel type radiators

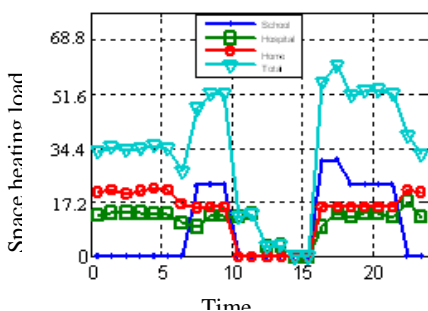


Fig.3 Estimated space heating load in three different buildings for one day in winter season
<https://doi.org/10.24084/repqj08.728>

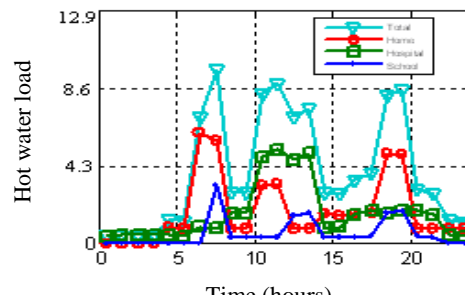


Fig. 5 Estimated hot water heating load in three different buildings for one day in winter season

C. Design of the Heat Exchanger

Most geothermal fluids, because of their elevated temperature, contain a variety of dissolved chemicals. These chemicals are frequently corrosive toward standard materials of construction. As a result, it is advisable in most cases to isolate the geothermal fluid from the process to which heat is being transferred. The task of heat transfer from the geothermal fluid to a closed process loop is most often handled by a plate heat exchanger. The most common type used in geothermal applications is the brazed plate heat exchanger. A number of characteristics particularly attractive to geothermal applications are responsible for this. Among these are:

1. Superior thermal performance
2. Availability of a wide variety of corrosion resistant alloys.
3. Ease of maintenance
4. Expandability and multiplex capability
5. Compact design

As shown in Fig.6 (a), the plate heat exchanger is basically a series of individual plates pressed between two heavy end covers. The entire assembly is held together by the tie bolts. Individual plates are hung from the top carrying bar and are guided by the bottom carrying bar. For single-pass circuiting, hot and cold side fluid connections are usually located on the fixed end cover. Multi-pass circuiting results in fluid connections on both fixed and moveable end covers. The brazed plate unit as shown in Fig.6 (b) eliminates the end plates, bolts, and gaskets from the design. Instead, the plates are held together by brazing with copper. This results in a much less complicated, lighter weight and more compact heat exchanger.

The key parameter in the selection process is the heat transfer area required to accomplish this task. The general formula below describes this situation [5].

$$Q = U * A * LMTD * Cf \quad (3)$$

Where:

- Q = Total heat load in k.cal /hr
- U = Overall heat transfer coefficient in k.cal /hr.m².oC
- A = Area (m²)

LMTD = Log mean temperature difference (oC)

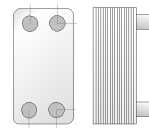
Cf = LMTD correction factor (0.85 - 1.0 for most geothermal applications).

The log mean temperature difference is calculated using the difference between the entering and leaving temperatures of the two fluids shown in Fig.6 (c) according to the following relationship

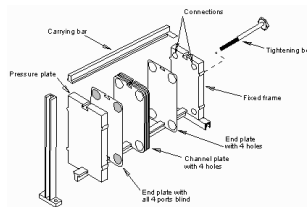
$$LMTD = \frac{\Delta t_1 - \Delta t_2}{\ln \left(\frac{\Delta t_1}{\Delta t_2} \right)} \quad (4)$$

$$\Delta t_1 = t_{out1} - t_{in2} \quad (5)$$

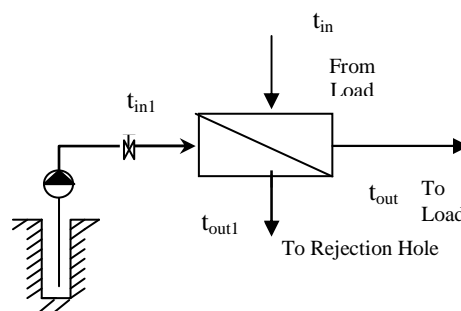
$$\Delta t_2 = t_{in1} - t_{out2} \quad (6)$$



(a)The plate heat exchanger.



(b)Brazed plate heat exchanger



(c)Entering and leaving temperatures of the two fluids.

Fig.6 The heat exchanger

D. Hot Water and Space Heating System Design Procedure

The design of the proposed system is summarized in the following steps:

Step 1. determine the space heating load required for each room in the three buildings using Eqs. (1)&(2)

Step 2. calculate the radiator heating area and radiator dimensions using Tables 1&2

Step3 use the hot water consumption in each building illustrated in Table 3 to determine the hot water load and the water heater capacity in each building .

Step 4 use the value of the total heat load (space heating load + water heating load) to calculate the heat transfer area required for the selected heat exchanger using Eqs (3),(4) & (5)

4. Results And Discussions

The Specifications of different components of the geothermal hot water and space heating system are illustrated. Different specifications of the geothermal water heater are included in Table 4. The design heat loss calculations for the library in the school building as example are shown in Table5. The area, the complete dimensions of the selected radiators needed in each room and the corresponding heat load in the three building is shown in Tables 6, 7 and 8 respectively.

5. Conclusion

The geothermal hot water and space heating system is the best and clean system to satisfy the energy needs in remote area buildings. We conduct a design analysis of the geothermal

heating system components and apply to the Umm Huweitat well in eastern desert as a case study. The design parameters and specifications of each component are illustrated.

Table 4 Specifications of different constituents of the geothermal water heater.

	Specification
a- Hot water tank	
• - Material	Stainless steel
• - Volume	1200 liter for home 900 liter for hospital 500 liter for school
Dimensions	240 cm *80 cm for home 225 cm *75cm for hospital 180 cm *60 cm for school
b-Insulation	
Type	Glass wool
• Thermal conductivity	9.024 *10 ⁻³ k.cal/ hr.m °C
• Thickness	7 cm
• Density	13 Kg/m ²
c-Heat exchanger	steel

Table 5 Design heat loss calculations for the library in school building

Fabric Heatloss									
Surface		Area		Temperature difference		U Value		Heat loss	Total
		m ²		°C		k.cal/hr.m ² .°C		k.cal/hr	k.cal/hr
External wall		41.58	x	14	x	0.791	=	461	
Ceiling		36	x	14	x	1.393	=	702	
window		4.32	x	14	x	4.3	=	260	
Floor		36	x	14	x	0.31	=	156	1579
Ventilation Heat loss									
air changes number		Room Volume		Temperature difference		Heat capacity of air		Heat loss	
		m ³		°C		k.cal/hr.m ³ .°C		watts	
1	x	118.8	x	14	x	0.284	=	472	472
Total Design Heat loss									2051

Table 6 Typical space heating load and radiator specifications for school building

Room Description	Room area (m ²)	Estimated heat load (kcal/hr) *10 ³	Design heat load (kcal/hr) *10 ³	Radiator Type	Heater Area (m ²)	Radiator Dimensions (mm)		
						Depth	Length	Height
Mosque and library	6*6	2.05	2.06	Steel tubular with headers	1.968	98	1968	1000
Class rooms, teacher rooms, music room, and computer room	4.8*6	1.78	1.806	Steel tubular with headers	1.722	98	1722	1000
Director room	6*8.	2.347	2.322	Steel tubular with headers	2.214	98	2214	1000
Reception	2.4*6	0.959	0.946	Steel tubular with headers	0.902	98	902	1000
Center corridor	2.4*6	0.533	0.516	Steel tubular with headers	0.492	98	492	1000
Kitchen	3*4.8	0.96	0.946	Steel tubular with headers	0.902	98	902	1000
W.C.	4.5*4.8	1.255	1.29	Steel tubular with headers	1.23	98	1230	1000
Right and left corridors	16*2.4	1.652	1.634	Steel tubular with headers	1.558	98	1558	1000

Table 7 Typical space heating load and radiator specifications for hospital building.

Room Description	Room area (m ²)	Estimated heat load (kcal/hr) *10 ³	Design heat load (kcal/hr) *10 ³	Radiator Type	Heater Area (m ²)	Radiator Dimensions (mm)		
						Depth	Length	Height
Reception	4*4	1.388	1.374	Steel tubular with headers	1.312	98	1312	1000
Waiting room and Examination rooms	4*4	1.138	1.118	Steel tubular with headers	1.044	98	1044	1000
Surgey room	4*4	1.387	1.348	Steel tubular with headers	1.474	98	1474	1000
Intensive care room	4.2*4.8	1.108	1.118	Steel tubular with headers	1.044	98	1044	1000
Nursing room and kitchen	3*4.8	0.581	0.402	Steel panel with coil	1.449	33	1410	900
Patient room 1	4.8*4	1.372	1.374	Steel tubular with headers	1.312	98	1312	1000
Patient room 2	4.8*4	1.303	1.390	Steel tubular with headers	1.330	98	1330	1000
Pharmacy	3.4*4.8	1.2	1.204	Steel tubular with headers	1.148	98	1148	1000
Bathrooms 1 & 2	3*4.8	0.433	0.402	Steel panel with coil	1.449	33	1410	900
Examination room	4.2*4.8	0.982	0.944	Steel tubular with headers	0.902	98	902	1000
Store room	2.4*2.4	0.279	0.238	Steel panel with coil	0.421	33	490	900
Main corridor	3*18.4	2.421	2.408	Steel tubular with headers	2.294	98	2294	1000
Secondary corridor	2.4*22	1.784	1.548	Steel tubular with headers	1.474	98	1474	1000
Entrance	3.4*4.8	0.383	0.402	Steel tubular with headers	0.374	98	374	1000

Table 8 Typical space heating load and radiator specifications for home building

Room Description	Room area (m ²)	Estimated heat load (kcal/hr) *10 ³	Design heat load (kcal/hr) *10 ³	Radiator Type	Heater Area (m ²)	Radiator Dimensions (mm)		
						Depth	Length	Height
Bed room 1	3.6*4.2	1.025	1.032	Steel tubular with headers	0.984	98	984	1000
Bed room 2	3.6*4.2	0.839	0.860	Steel tubular with headers	0.820	98	820	1000
Bathroom	2.4*2.4	0.369	0.344	Steel panel with coil	0.828	35	920	900
Kitchen	2.1*3	0.514	0.516	Steel panel with coil	1.242	35	1380	900
Living room	3.6*4.2	0.764	0.774	Steel tubular with headers	0.738	98	738	1000
Corridor	1.2 *6	0.713	0.688	Steel tubular with headers	0.656	98	656	1000

Table 9 Plate heat exchanger design – parameters.

Item	Specification
Type	brazed plate heat exchanger
Fouling factor	0.0001 to 0.0002
Resulting overall heat transfer coefficient	4443- 5615 k. cal/hr. m ² .°C
Heat transfer surface area(m ²)	2.648
Number of plates	19
Plate material	Stainless Steel

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