

Frequency constrained unit commitment in isolated power systems with high penetration of RES

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Introduction

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• There are **thousands of isolated power systems** worldwide and their number is increasing (e.g., off-grid systems).



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Source: P. Blechinger, R. Seguin, C. Cader, P. Bertheau, Ch. Breyer, Assessment of the Global Potential for Renewable Energy Storage Systems on Small Islands, Energy Procedia, Volume 46, 2014.

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Introduction

- Isolated power systems are especially sensitive to active power unbalances due to their:
 - isolated nature (lack of supporting interconnections)
 - the small number of committed generation units, with relatively large individual generation levels and reserve requirements.
 - spatially concentrated variable RES
- They are thus per se low-inertia power systems.

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 Large active power unbalances (e.g., generation outages) lead to frequency deviations, confined by the primary frequency control (PFC) activating the spinning reserve.





- The **objective of operation planning** is to supply the electrical demand at minimum variable cost such that, among others, **security of supply** is guaranteed.
- To guarantee security of supply, a certain amount of spinning reserve is hold back for the PFC and secondary frequency control.
- The amount of spinning reserve basically follows a static N-1 criterion, although frequency stability is of course a dynamic problem.



Introduction

- Currently, the spinning reserve is mainly provided by synchronous generation (e.g., thermal and hydro generation).
- The growing penetration of RES generation affects reserve provision and frequency stability by substituting synchronous generation,
 - reducing further the available resources for spinning reserve.
 - reducing further the available inertia and PFC capacity.



- Questions arise such as:
 - What if **RES generation started providing spinning reserve**? Is it viable? Is it feasible?
 - What if the determination of the amount of spinning reserves followed dynamic criteria? What are these criteria? How can be frequency stability included into the planning problem? What formulations should be used to be efficient? Transparent?



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RES generation providing spinning reserve

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- Currently, RES generation does not provide down- or upwards spinning reserve.
- Grid codes require the ability to provide PFC, but this is not tantamount to a mandatory and planned provision of PFC.
- Providing spinning reserve could be an option to further foster RES penetration instead of simply spillingt it at high penetration levels.



• The idea is to avoid using conventional generation that is just providing spinning reserve but making use of RES generation.



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Source: Rajabdorri, M., et al.: Viability of providing spinning reserves by RES in Spanish Island power systems. IET Renew. Power Gener. 2021; 15: 2878–2890.



 The unit commitment formulation, minimizing variable operation costs, needs to be modified by considering a possible deloaded operation:

$$\begin{split} \min_{x,P} suc(x_{g,t}) + gc(P_{g,t}) & \min_{x,P} suc(x_{g,t}) + gc(P_{g,t}) \\ \sum_{g \in G} P_{g,t} = D_t & \sum_{g \in G} P_{g,t} = D_t \\ \hline P_{g,t} = \overline{P}_{g,t} = W_{g,t} \cdot x_{g,t} \quad \forall g \in W \subset G & \overline{P}_{g,t} = W_{g,t} \quad \forall g \in W \subset G \\ \hline P_{g,t} \cdot x_{g,t} \leq P_{g,t} \leq \overline{P}_{g,t} \cdot x_{g,t} & \frac{P_{g,t} \cdot x_{g,t}}{\vdots} & \frac{P_{g,t} \cdot x_{g,t}}{\vdots} \\ \sum_{g \in G \setminus W, g \neq gg} \left(\overline{P}_{g,t} - P_{g,t} \right) \geq L_{gg} \cdot P_{gg,t} & \sum_{g \in G, g \neq gg} \left(\overline{P}_{g,t} - P_{g,t} \right) = L_{gg} \cdot P_{gg,t} \\ \end{split}$$
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• Impact of providing down- and upwards reserve on variable operation costs, and RES generation spillage:





 Impact of high-RES generation scenario providing spinning reserve on frequency stability:



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D. Fuentes Pascual, M. Rajabdorri, L. Sigrist, E. Lobato, Technical impacts of providing frequency regulation by wind turbines in Spanish island power systems, November 2022.



Frequency constrained unit commitment (FCUC)

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- Currently, the reserve criterion is a static one, although related frequency stability is a dynamic problem.
- FCUC formulations explicitly consider frequency stability constraints.
- Different approaches exist, but they coincide in estimating certain indexes related to the underlying frequency dynamics.



- Commonly, three indexes are considered:
 - Initial rate-of-change of frequency (RoCoF)
 - Steady-state frequency, f_{ss}
 - Frequency nadir, f_{nadir}





- FCUC approaches can be broadly grouped into analytical or data-driven approaches:
 - Analytical approaches include explicit expressions for RoCoF, nadir and steady-state frequency
 - Data-driven approaches estimate them through functions deduced from a large training set.

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Analytical FCUC

• In a analytical approach, the standard UC formulations is extended by adding the following terms (here, for generation outages):

$$\Delta \dot{f}\Big|_{t=t_0} \ge \Delta \dot{F}_{ini} \qquad 2 \cdot \left(\sum_{g,g \neq gg} H_g \cdot x_{g,t}\right) \cdot \Delta \dot{F}_{ini} \le -p_{gg,t}$$

$$\Delta f\Big|_{t=\infty} \ge \Delta F_{ss} \qquad \left(\sum_{g,g \neq gg} K_g \cdot x_{g,t}\right) \cdot \Delta F_{ss} \le -p_{gg,t}$$

$$\Delta f\left(t\right) \ge \Delta F_{nadir} \qquad \left(\Delta F_{nadir}\right)^2 \left[2 \cdot \left(\sum_{g,g \neq gg} \frac{K_g}{T_g} \cdot x_{g,t}\right) \cdot \left(\sum_{g,g \neq gg} H_g \cdot x_{g,t}\right)\right] \le p_{gg,t}^2$$
A. Rouco, M. Rajabdorri, E. Lobato, L. Sigrist, Analytical frequency-constrained UC for island power systems, 15th EFE PowerTach Conference, PowerTach 2023. Betrade (Serbia), 25,29 June 2023.

15th IEEE PowerTech Conference - PowerTech 2023, Belgrade (Serbia). 25-29 June 2023.



Analytical FCUC

• Application of the FCUC to a Spanish isolated power system







Analytical FCUC

• Comparison with standard UC

	Cost (k€)	Spillage (MWh)	Average ∆f _{nadir} (Hz)	Average shed load (MW)
FCUC	156	14.1	-0.88	0.8
standard UC	141	2.8	-0.93	1.2





• In a data-driven approach, a three-step approach can be used:



Creation of the **training set** by considering all large amount of scenarios and contingencies.

Since the results are in **dichotomous form, Logistic Regression (LR)** can be used.

Explanatory variables, ξ, available within UC are: the inertia, the relative power loss, the reserve, etc.

$$c_0 + c_1 \xi_{1,gg} + c_2 \xi_{2,gg} + \dots + c_m \xi_{m,gg} \ge \psi$$



 Logistic regression (LR) predicts the probability of a result of being acceptable or not in terms of the explanatory variables, ξ_i.





• If we look at the logarithm of the corresponding odds of being acceptable or not in terms of the explanatory variables, ξ_i :





 Application of the data-driven FCUC to a Spanish isolated power system and comparison with the standard UC

	HQFR (%)	LQFR (%)	average F _{nadir} (Hz)	Average shed load (MW)	Operation cost (k€)
standard UC	68	32	48.29	2.3	141
FCUC ψ = 0	81	19	48.77	1.2	144
FCUC ψ = -2.12	79	21	48.68	1.5	143
FCUC ψ = -6.91	77	23	48.52	2.1	140





• Impact on frequency dynamics







Concluding remarks



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Concluding remarks

- Currently, the amount of spinning reserve follows a static N-1 criterion although the underlying problem is dynamic.
- RES generation does not provide upwards spinning reserve.
- It has been shown that providing reserve by RES generation is beneficial from the technical and economic point of view (although the economic impact is more straightforward).
- It has been shown the a dynamic criterion can be set up by using either analytical or data-driven approaches. The more conservative the approach, the costlier the operation. comillas.edu